



**NORTH DAKOTA  
ASPHALT CONFERENCE**

**April 5-6, 2016 • Ramada Bismarck Hotel**

**Asphalt Binder Basics  
Specifications, History and Future**

**Mark D. Blow, PE  
Sr. Regional Engineer - Asphalt Institute  
Harrisburg, SD**

“A dark brown to black cementitious material in which the predominating constituents are bitumens which occur in nature or are obtained in petroleum processing.” – ASTM D8

*The glue that binds the aggregate together and waterproofs the pavement.*

First US hot mix asphalt (HMA) constructed in 1870's

- Pennsylvania Ave.
- Used naturally occurring asphalt from surface of lake on Island of Trinidad



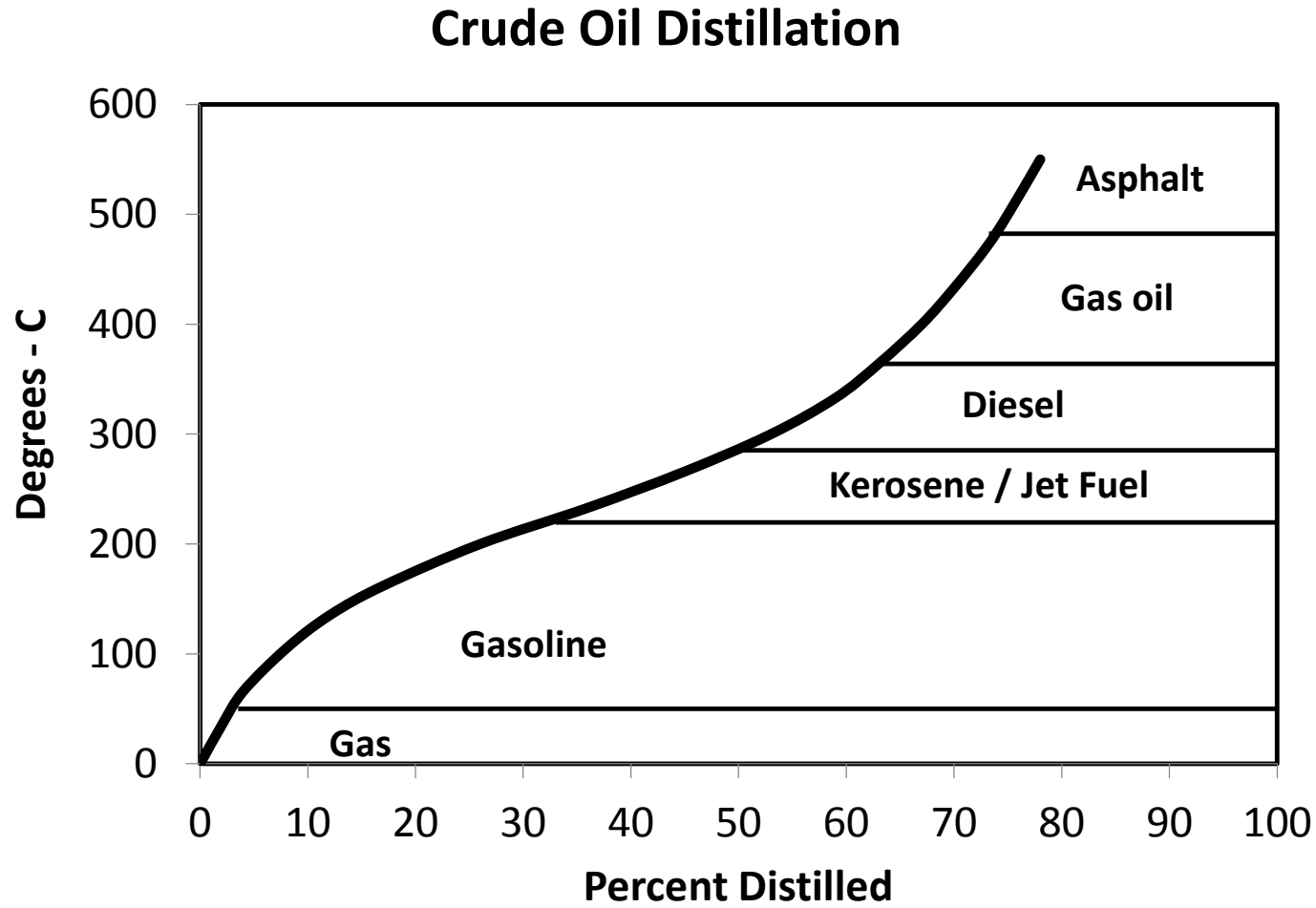
Demand for paved roads exceeded the supply of lake  
asphalts in late 1800's  
Led to use of petroleum asphalts





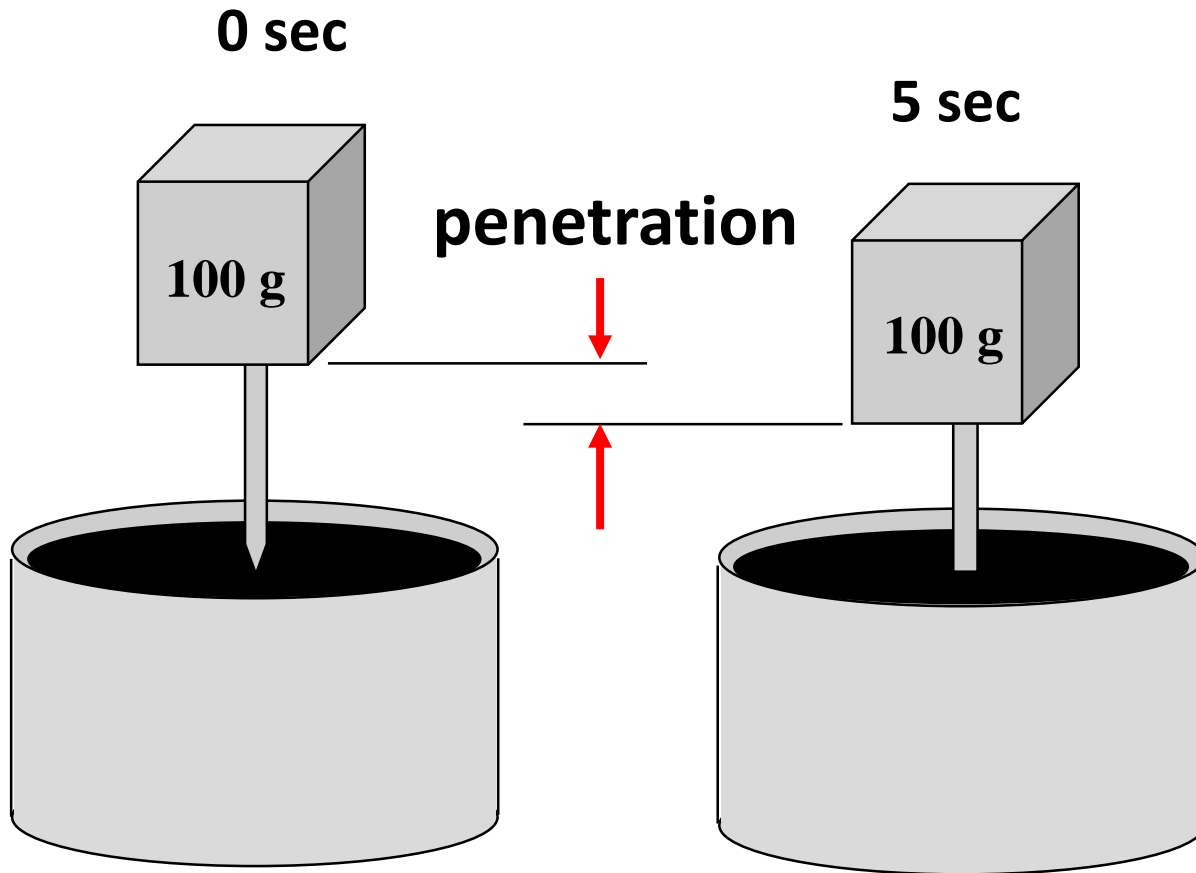
Sweet vs. Sour  
Light vs. Heavy

# Crude Distillation Temperatures



- Penetration
  - Developed in early 1900s (first ASTM 1947)
  - Tested @ 25°C (77°F)
- Viscosity
  - Developed in 1950s
  - Absolute Viscosity
    - Tested @ 60°C (140°F)
  - Kinematic Viscosity
    - Tested @ 135°C (275°F)

# Penetration (1900s)





## Penetration Specification

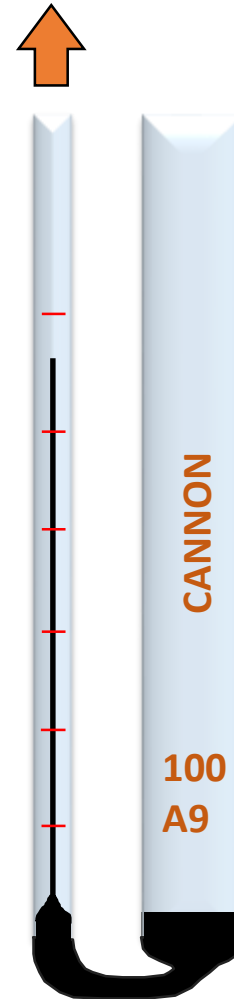
Characteristics	AASHTO	ASTM	Penetration Grades				
Penetration, 77°F, 100 g, 5 sec	T49	D5	40 - 50	60 - 70	85 - 100	120 - 150	200 - 300
Visc. @ 275°F Kinematic, Cs Saybolt Furol, SSF	T201	D2170 E102	240 + 120 +	200 + 100 +	170 + 85 +	140 + 70 +	100 + 50 +
Flash Point, °F, Clev Open Cup	T48	D92	450 +	450 +	450 +	425 +	350 +
Thin Film Oven Test Pen on Residue, 77°F, % Orig.	T179 T49	D1754 D5	55 +	52 +	47 +	42 +	37 +
Ductility @ 77°F, cm @ 60°F, cm	T51	D113	100 + -----	100 + -----	100 + -----	60 + -----	----- 60 +
Sol. In Trichloroethylene, %	T44	D2042	99.0 +	99.0 +	99.0 +	99.0 +	99.0 +

General Requirement – The asphalt shall be prepared by the refining of petroleum. It shall be uniform in character and shall not foam when heated to 350°F

# Viscosity (1950s)



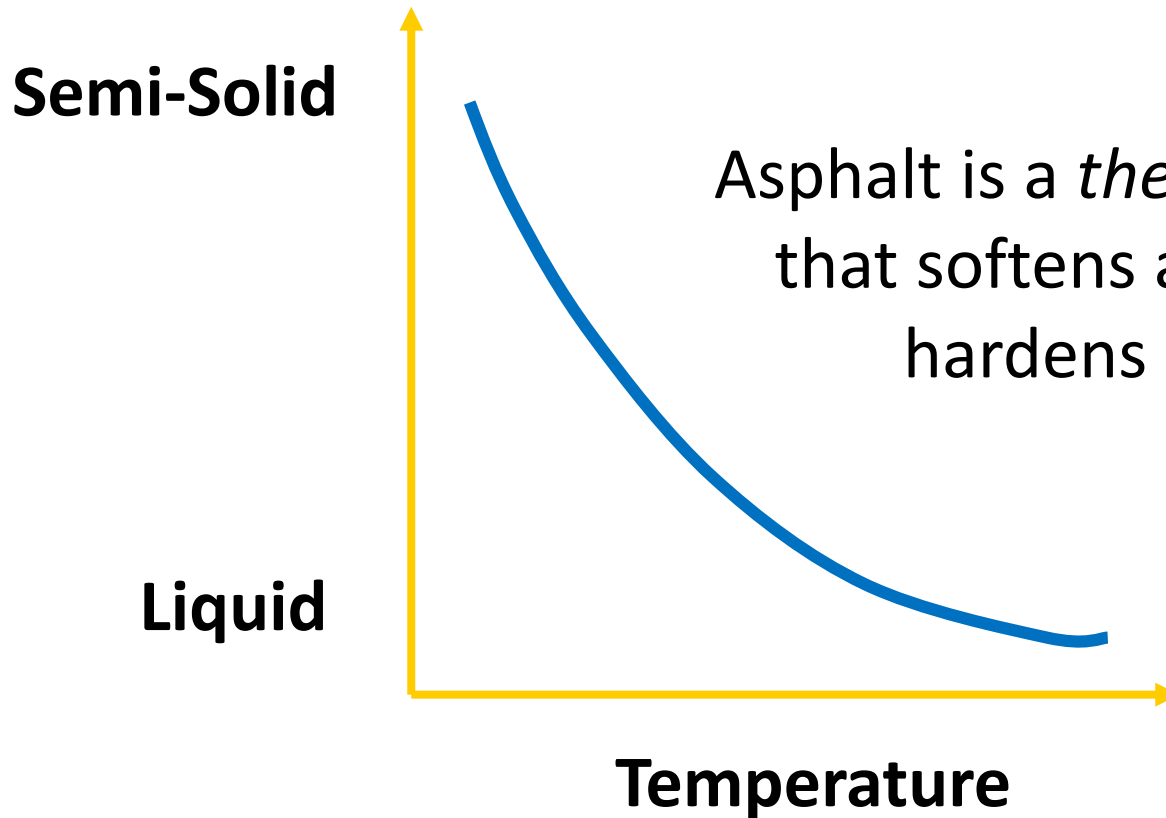
vacuum



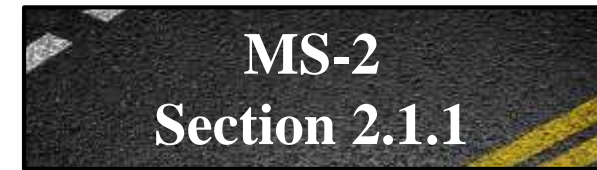
Measure  
time of flow  
between  
lines

## Viscosity Specification

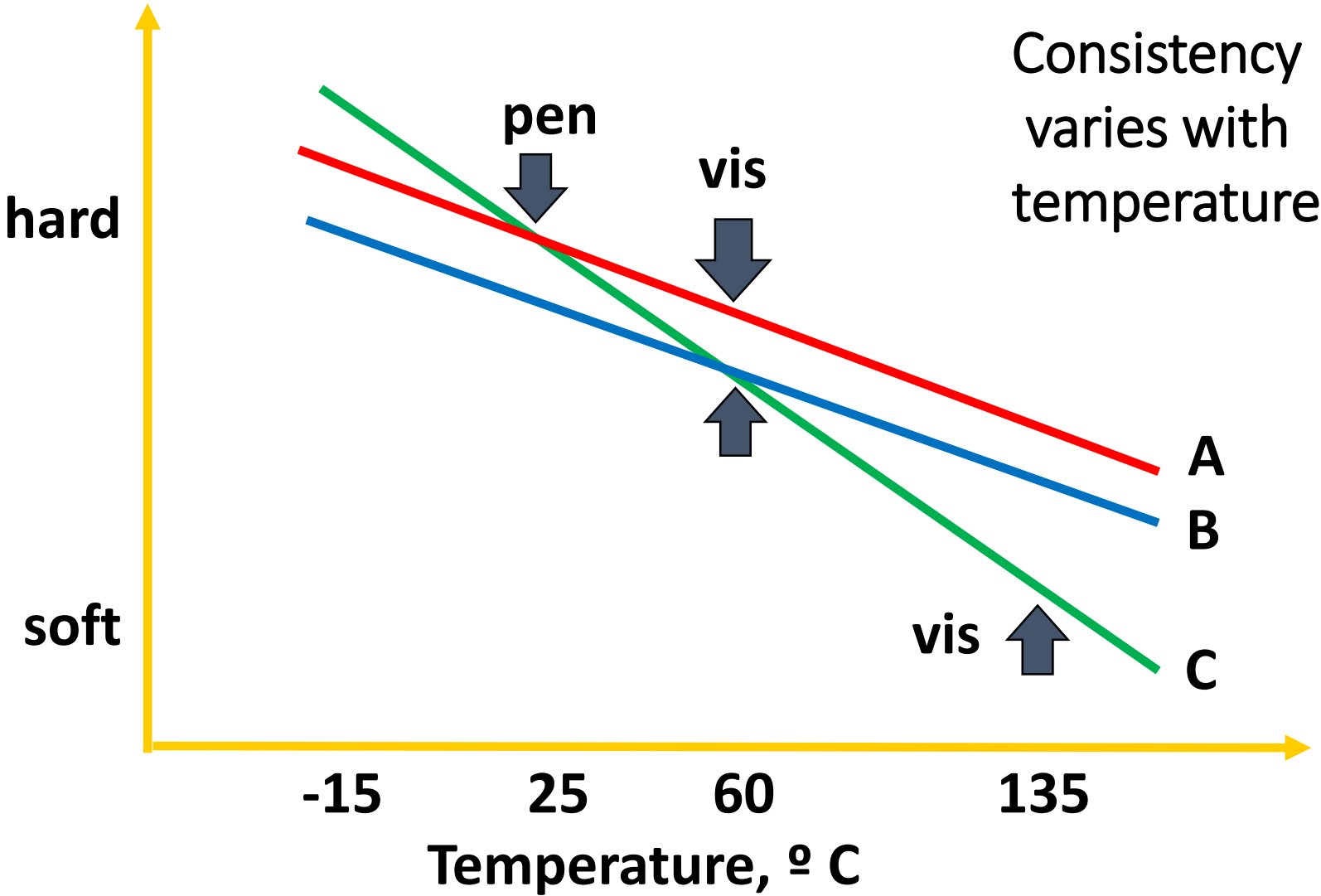
Characteristics	Viscosity Grades					
Test	AC-2.5	AC-5	AC-10	AC-20	AC-30	AC-40
Visc. @ 140°F Kinematic, P	250 ± 50	500 ± 100	1000 ± 200	2000 ± 400	3000 ± 600	4000 ± 800
Visc. @ 275°F Kinematic, Cs, Min.	125	175	250	300	350	400
Penetration, 77°F, 100 g, 5 sec, Min.	220	140	80	60	50	40
Flash Point, °F, C.O.C., Min.	325	350	425	450	450	450
Sol. In Trichloroethylene, %	T44	99.0 +	99.0 +	99.0 +	99.0 +	99.0 +
Tests on TFOT Residue						
Loss on Heating, %, Max.		1.0	0.5	0.5	0.5	0.5
Visc. @ 140°F Kinematic, P, Max.	1000	2000	4000	8000	12000	16000
Ductility @ 77°F, cm, Min.	100	100	75	50	40	25
Spot Test	Neg.	Neg.	Neg.	Neg.	Neg.	Neg.



Asphalt is a *thermoplastic* material that softens as it is heated and hardens when cooled.



# Historic Specifications - Shortcomings



## Grading System Based on Climate

**PG 58-22**

Performance  
Grade

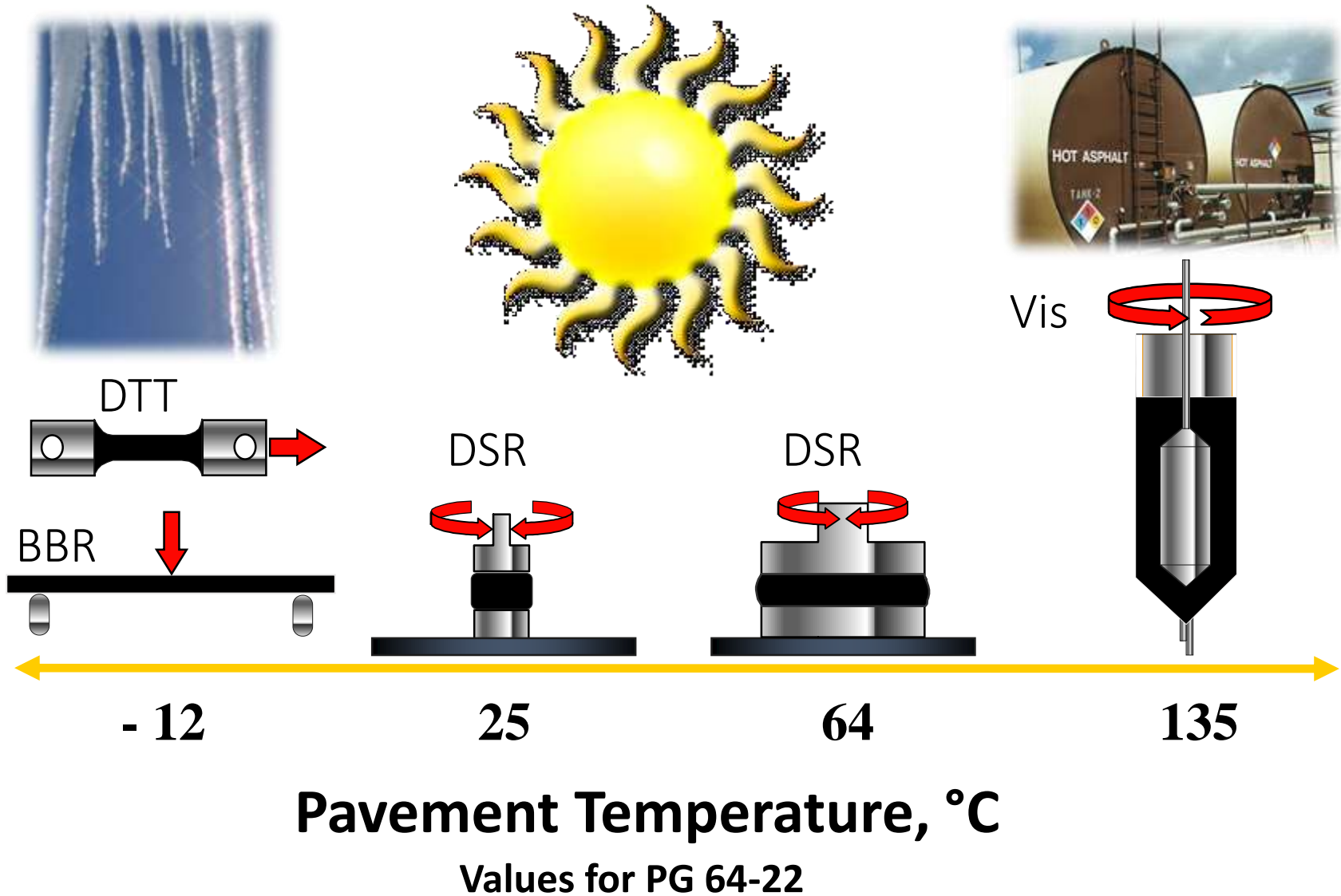
Average 7-day  
max pavement  
design temp

Min pavement  
design temp



MS-2  
Section 2.1.1

# Testing Temperature – Climate based

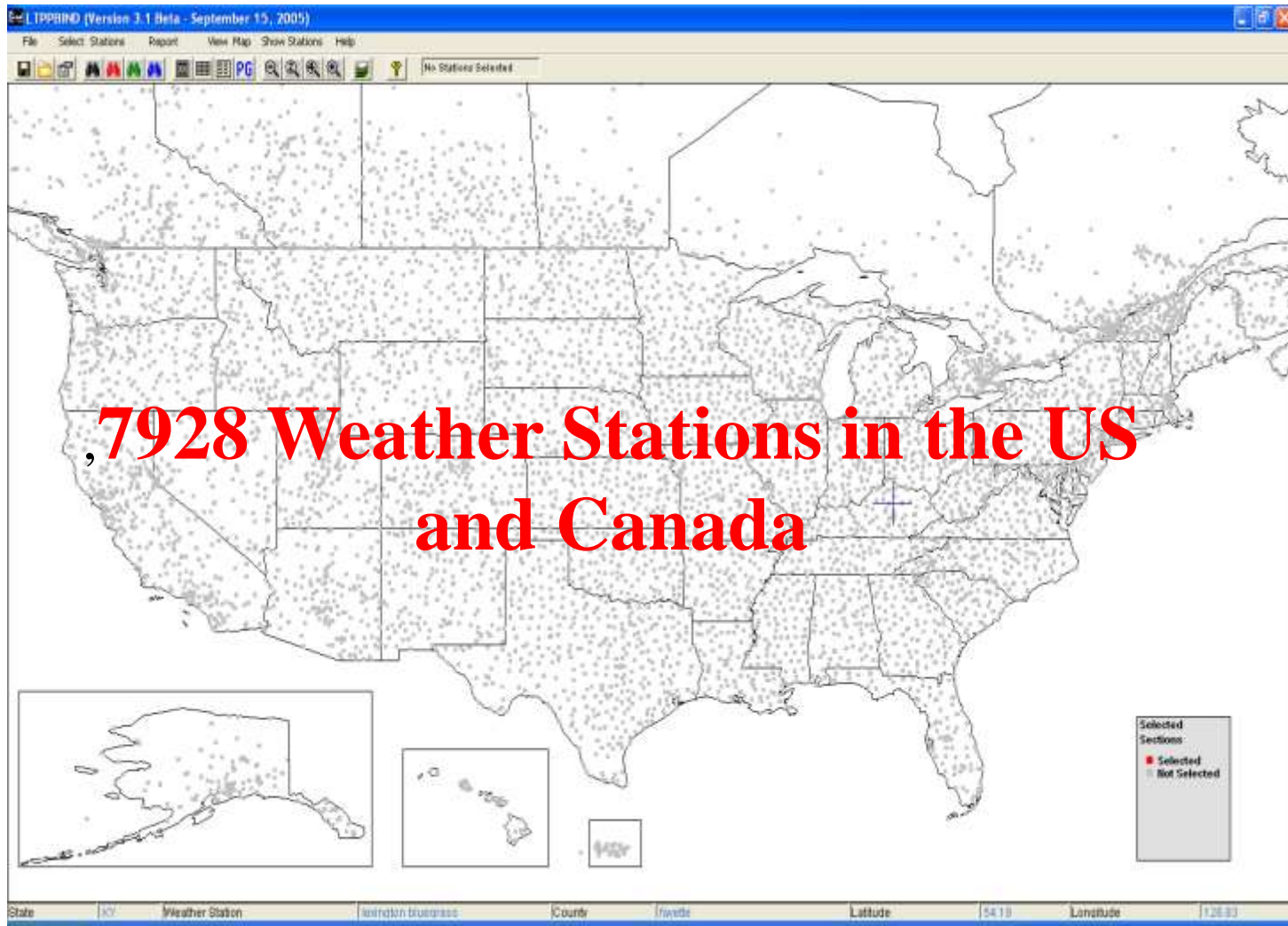


**Pavement Temperature, °C**

Values for PG 64-22

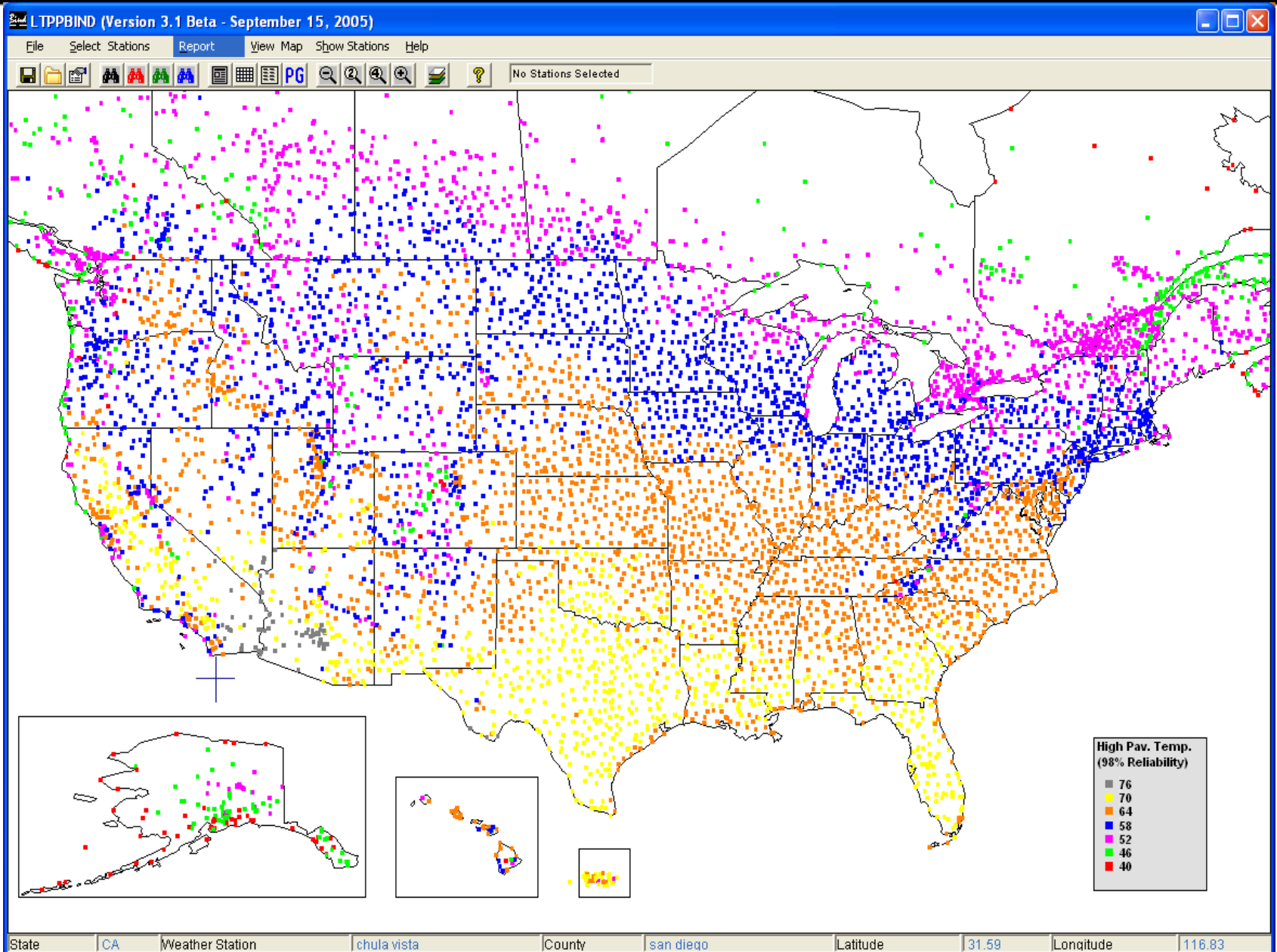
## LTPPBIND Software

<http://www.fhwa.dot.gov/PAVEMENT/ltp/ltpbind.cfm>

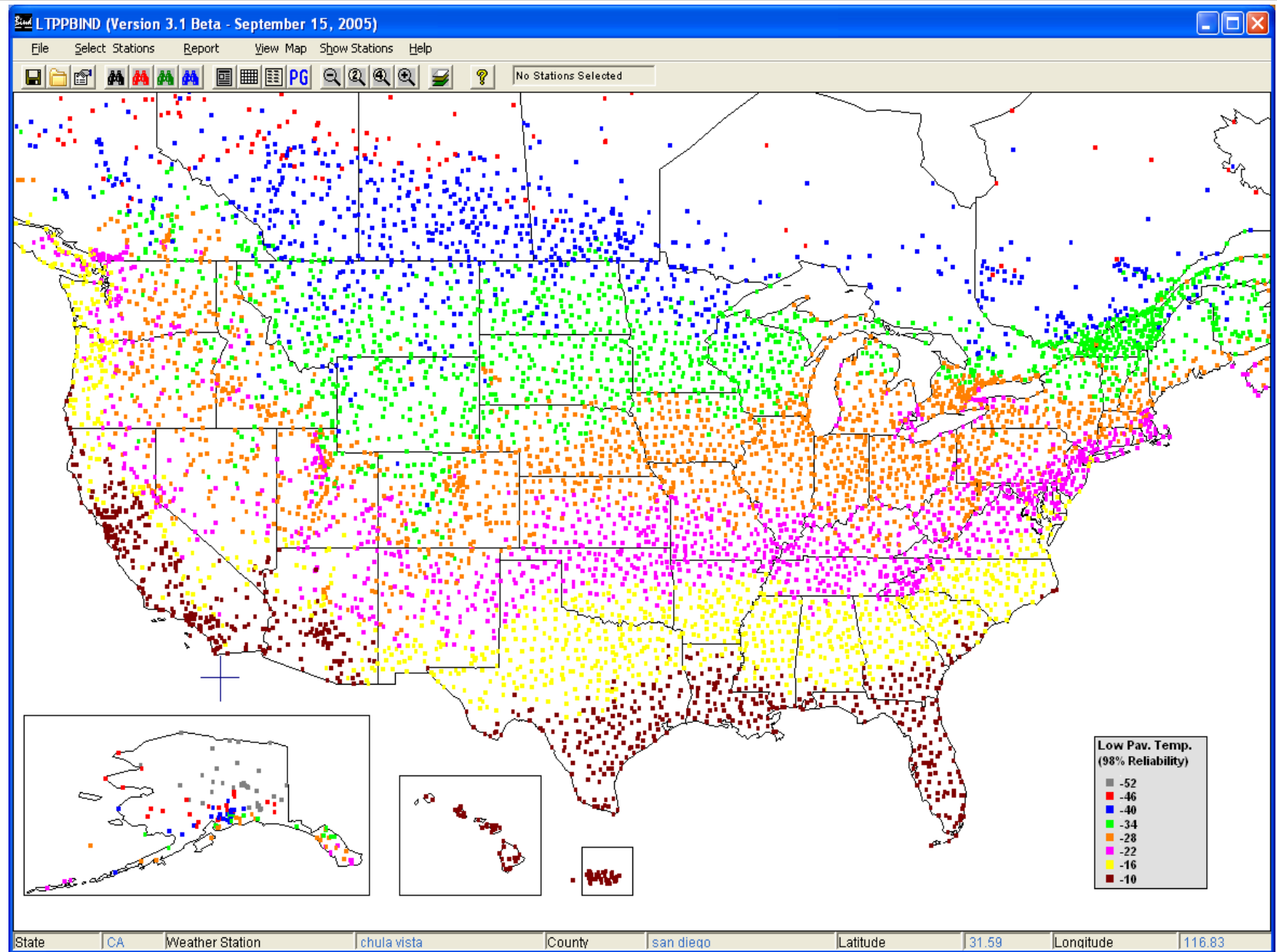


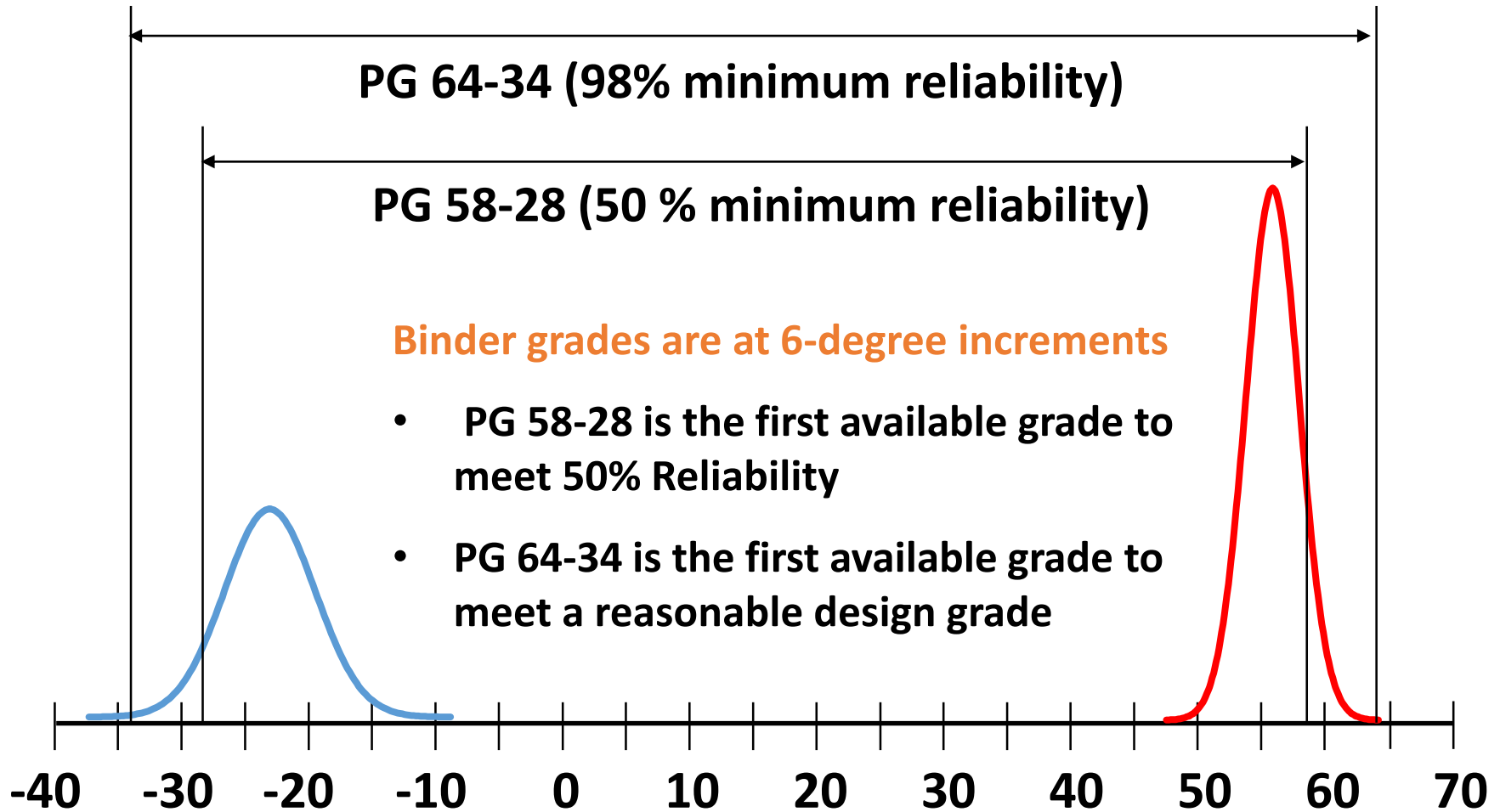


# High Temperature Grades

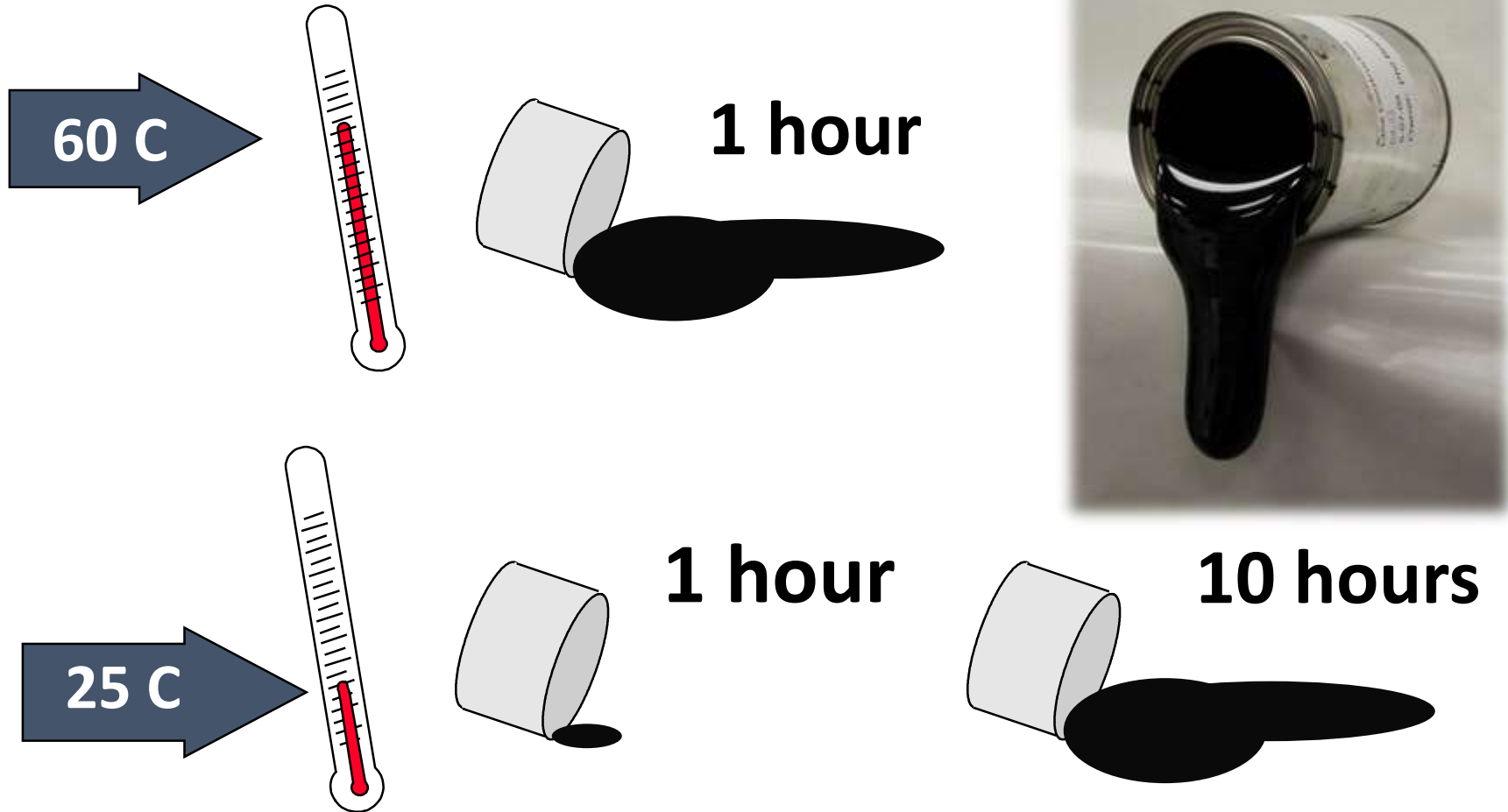


# Low Temperature Grades





## Time & Temperature Dependent





## Example:

- Toll road  
PG 64-22 ← 90 kph (55 MPH)
- Toll booth  
PG 70-22 ← Slow
- Weigh stations  
PG 76-22 ← Stopping

- 10 to 30 million ESALs
  - Consider increasing one high temperature grade
- > 30 million ESALs
  - Increase one high temperature grade
- Newer recommendations are based on more gradual bumping in LTPPBind version 3.0+



# Performance Grades

Max. Design Temp.	PG 46	PG 52				PG 58				PG 64				PG 70				PG 76				PG 82														
Min. Design Temp.	-34	-40	-46	-10	-16	-22	-28	-34	-40	-46	-16	-22	-28	-34	-40	-10	-16	-22	-28	-34	-40	-10	-16	-22	-28	-34	-10	-16	-22	-28	-34	-10	-16	-22	-28	-34

## Original

$\geq 230$ °C	<b>Flash Point</b>																											
$\leq 3$ Pa-s @ 135 °C	<b>Rotational Viscosity</b>																											
$\geq 1.00$ kPa	<b>DSR G*/sin <math>\delta</math></b> (Dynamic Shear Rheometer)																											
	46	52				58				64				70				76				82						

## (Rolling Thin Film Oven) RTFO, Mass Change $\leq 1.00\%$

$\geq 2.20$ kPa	<b>DSR G*/sin <math>\delta</math></b> (Dynamic Shear Rheometer)																											
	46	52				58				64				70				76				82						

## (Pressure Aging Vessel) PAV

20 hours, 2.10 MPa	90	90				100				100				100(110)				100(110)				100(110)															
$\leq 5000$ kPa	<b>DSR G* sin <math>\delta</math></b> (Dynamic Shear Rheometer) <span style="float: right;">Intermediate Temp. = [(Max. + Min.)/2] + 4</span>																																				
	10	7	4	25	22	19	16	13	10	7	25	22	19	16	13	31	28	25	22	19	16	34	31	28	25	22	19	37	34	31	28	25	40	37	34	31	28
$S < 300$ MPa $m \geq 0.300$	<b>BBR S (creep stiffness) &amp; m-value</b> (Bending Beam Rheometer)																																				
	-24	-30	-36	0	-6	-12	-18	-24	-30	-36	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	0	-6	-12	-18	-24

If BBR m-value  $\geq 0.300$  and creep stiffness is between 300 and 600, the Direct Tension failure strain requirement can be used in lieu of the creep stiffness requirement.

$\epsilon_t \geq 1.00\%$	<b>DTT</b> (Direct Tension Tester)																																				
	-24	-30	-36	0	-6	-12	-18	-24	-30	-36	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	0	-6	-12	-18	-24

# Is a PG a Modified Binder?

*Effect of Loading Rate*

*Reliability*

“Rule of 92”

**PG 64 - 34 => 64 - - 34 = 98**

**Probably modified**

*Depends on asphalt source*

*Rounding*

*Effect of Traffic*







The use of polymer modified binders has grown tremendously over the past several years

However, the most widely used binder specification in the U.S., AASHTO M320, was based on a study of neat (unmodified) binders, and may not properly characterize polymer modified binders

# Does PG Grading Predict Performance?

Study of the two mixes with the same aggregate structure, but different binders.

PG 63-22 modified, no rutting



PG 67-22 unmodified, 15mm rut



# What happened as a result of M 320's inability to fully characterize polymer-modified binders?

- Most states began requiring additional tests to the ones required in AASHTO M 320
- These mostly empirical tests are commonly referred to as “PG Plus” tests
- These tests are not standard across the states – difficult for suppliers
- Even some of the tests that are the most common, e.g. Elastic Recovery, are not run the same way from state to state

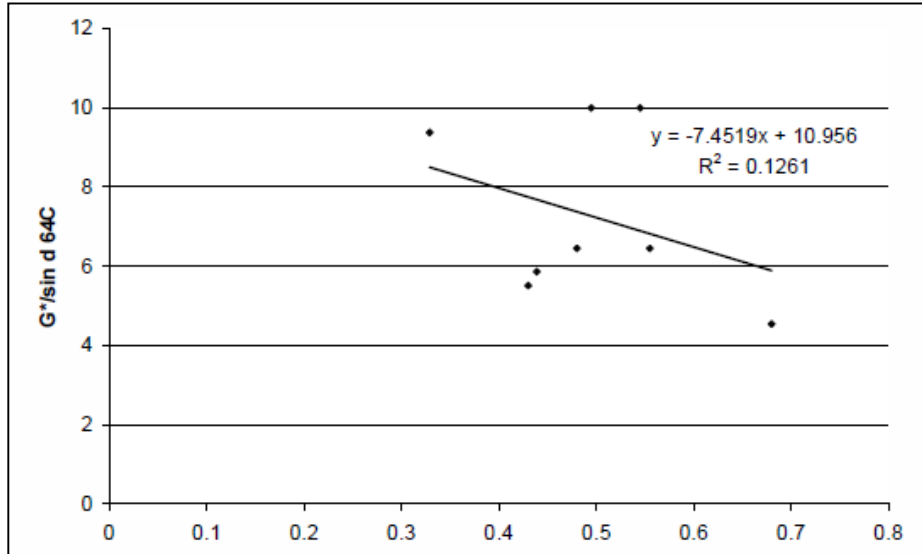
- The Elastic Recovery Test is an excellent tool to establish the *presence* of polymer modification.
  - It takes about 4 hours to prepare and test samples for this information.
- However, it is a poor tool to evaluate the rutting *performance* of polymer-modified binders.
- The MSCR test can use the same sample already being run in the DSR to give more information in a few extra minutes.

- Performed on RTFO-aged Binder
- Test Temperature
  - Environmental Temperature
  - Not Grade-Bumped
- 10 cycles per stress level
  - 1-second loading at specified shear stress
    - 0.1 kPa
    - 3.2 kPa
  - 9-second rest period

- The pavement was heated to a constant 64°C.
- The FHWA ALF uses an 18,000 lb. single wheel load with no wheel wander.
- The speed is 12 MPH.
- This is an extreme loading condition far more severe than any actual highway.

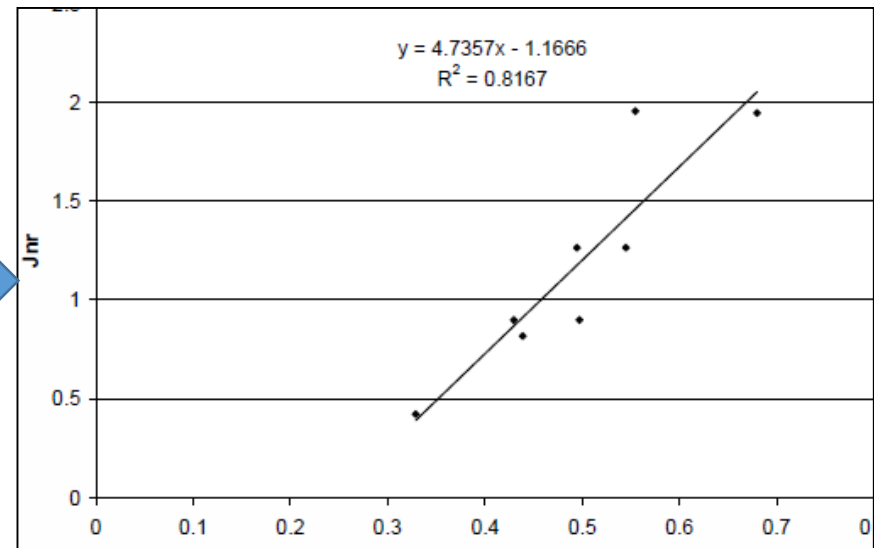


# ALF Loading – M 320 vs. M 332



← Traditional M 320  
PG Spec  
 $R^2 = 0.13$

New M 332  
PG Spec  
 $R^2 = 0.82$



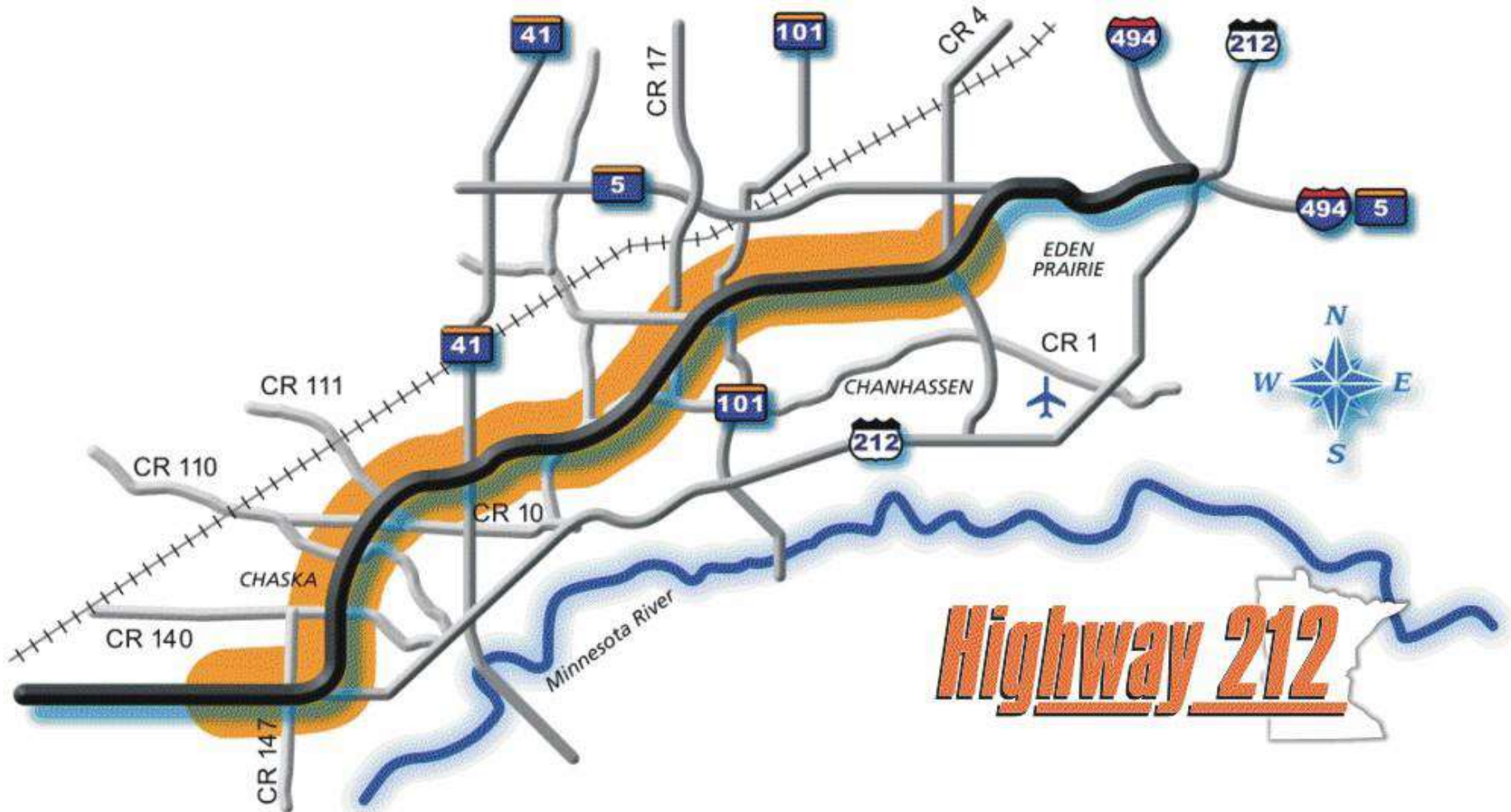


# Performance Grades (AASHTO M332)

High PG	PG 52						PG 58					PG 64					PG 70					PG 76							
Low PG	-10	-16	-22	-28	-34	-40	-46	-16	-22	-28	-34	-40	-10	-16	-22	-28	-34	-40	-10	-16	-22	-28	-34	-40	-10	-16	-22	-28	-34
<b>Original</b>																													
$\geq 230$ °C	<b>Flash Point, AASHTO T 48</b>																												
$\leq 3$ Pa-s	<b>Rotational Viscosity @ 135° C, AASHTO T 316</b>																												
$\geq 1.00$ kPa	SHVE	<b>DSR <math>G^*/\sin \delta</math> (Dynamic Shear Rheometer), AASHTO T 315</b>																											
		52						58					64					70					76						
<b>RTFO (Rolling Thin Film Oven), AASHTO T 240</b>																													
$\leq 1.00\%$	<b>Mass Change</b>																												
$\leq 4.5$ kPa <sup>-1</sup> $\leq 2.0$ kPa <sup>-1</sup> $\leq 1.0$ kPa <sup>-1</sup> $\leq 0.5$ kPa <sup>-1</sup>	SHVE	<b>MSCR <math>J_{nr, 3.2}</math> (Multiple Stress Creep-Recovery), AASHTO T 350</b>																											
		52						58					64					70					76						
$\leq 75\%$	SHVE	<b>MSCR <math>J_{nr, Diff}</math> (Multiple Stress Creep-Recovery), AASHTO T 350</b>																											
		52						58					64					70					76						
<b>PAV (Pressure Aging Vessel), AASHTO R28</b>																													
	90						100					100					100(110)					100(110)							
$\leq 5000$ kPa $\leq 6000$ kPa $\leq 6000$ kPa $\leq 6000$ kPa	SHVE	<b>DSR <math>G^*\sin \delta</math> (Dynamic Shear Rheometer), AASHTO T 315</b> Intermediate Temp. = [(High PG + Low PG)/2] + 4																											
		25	22	19	16	13	10	7	25	22	19	16	13	31	28	25	22	19	16	34	31	28	25	22	19	37	34	31	28
$S \leq 300$ MPa $m \geq 0.300$	<b>BBR S (creep stiffness) &amp; m-value (Bending Beam Rheometer), AASHTO T 313</b>																												
	0	-6	-12	-18	-24	-30	-36	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	-30	0	-6	-12	-18	-24	-30	0	-6	-12	-18	-24

• If BBR m-value  $\geq 0.300$  and creep stiffness is between 300 and 600, the Direct Tension failure strain requirement of  $\geq 1.00\%$  can be used in lieu of the creep stiffness requirement.  
 • Binder shall be homogeneous, free from water, contain no deleterious materials, be at least 99.0% soluble and contain no particles larger than 250  $\mu\text{m}$ .





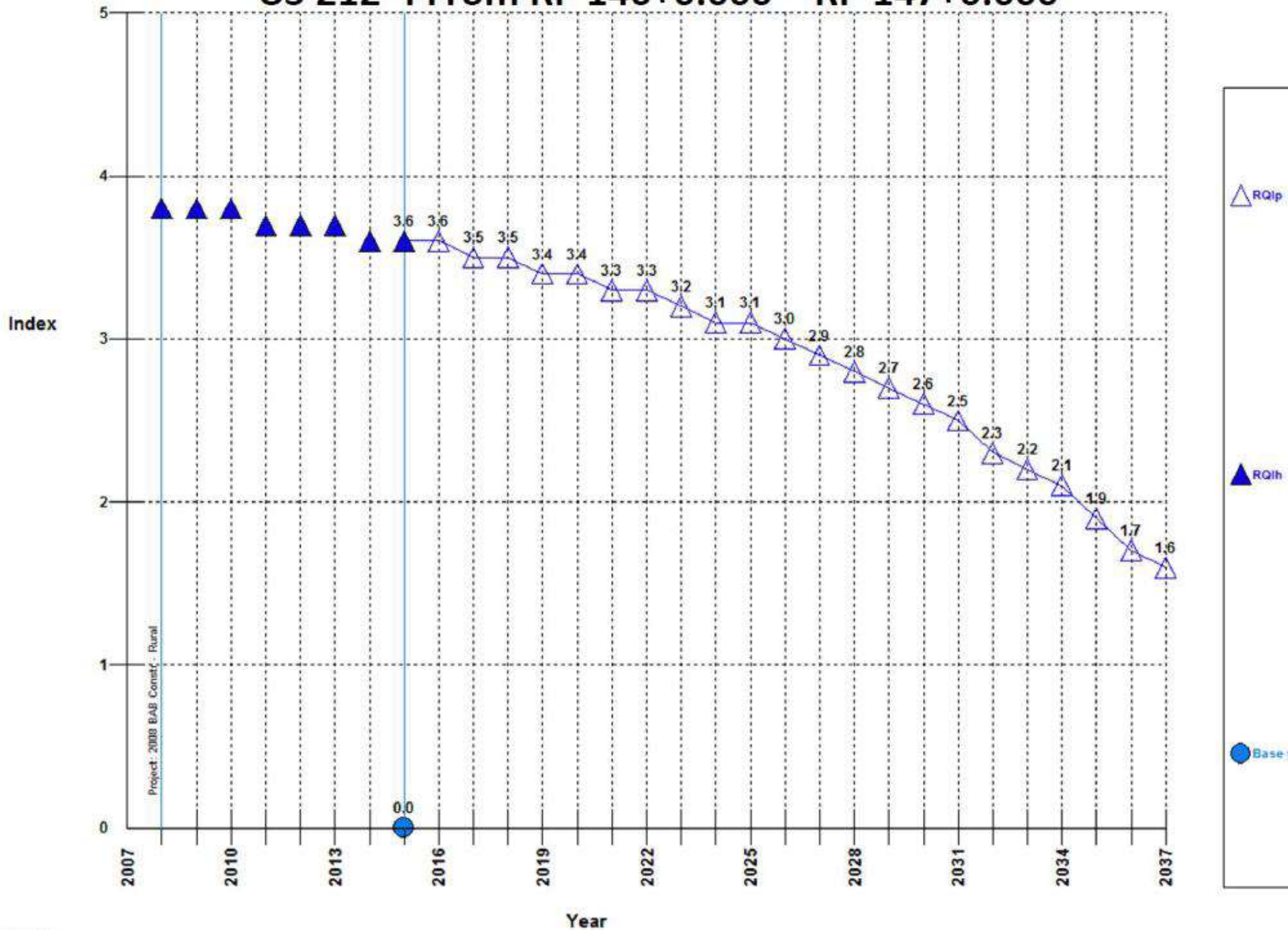
Chris Kufner, MnDOT  
Metro District Pavement & Materials Engineer

# Performance of US 212 SMA

- ▶ > 10 million ESALs → Concrete Pavement
- ▶ < 10 million ESALs → LCCA → Alternate Bid
  
- ▶ Majority of project was > 10 million, but
- ▶ Westerly 2.7 miles < 10 million ESALs
  
- ▶ Alternate Bid:
  - Bituminous option: 9" Bit (top 2" is SMA)
  - Concrete option: 10" Concrete
    - BOTH: 6" Aggregate Base over 24" Sel Granular over 24" compaction subcut.

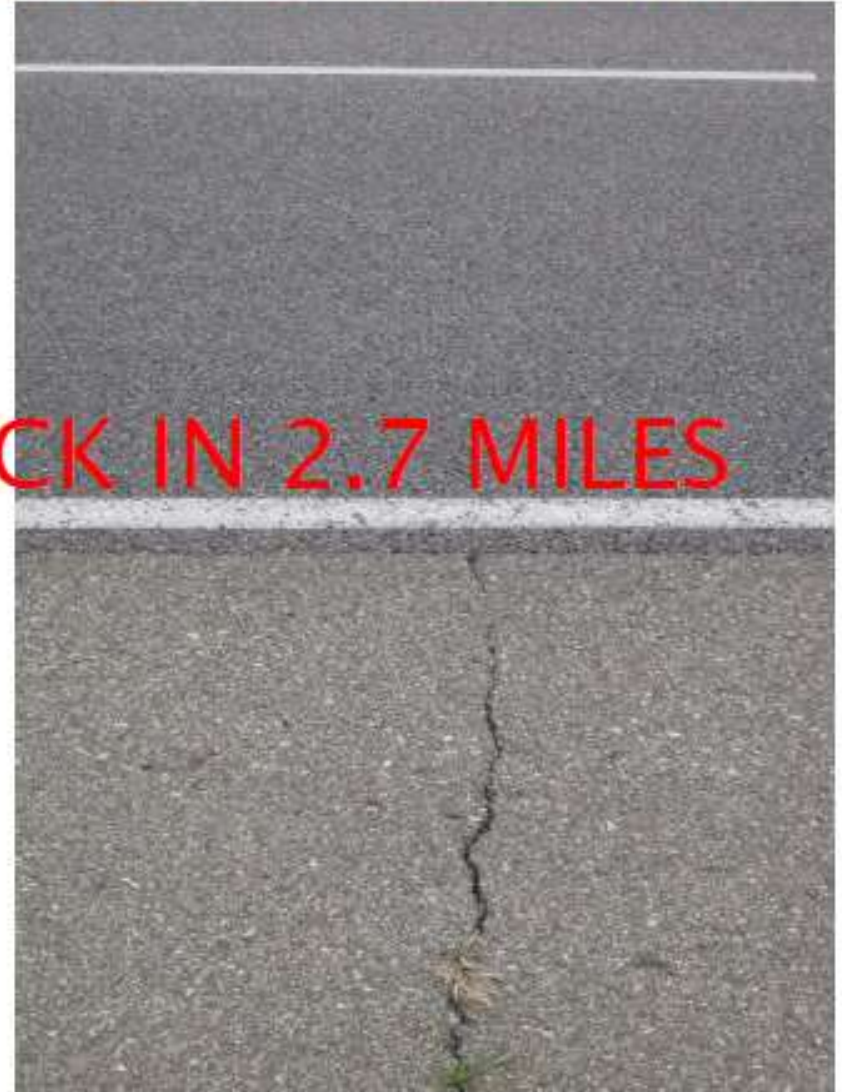


# US 212- I From RP 146+0.000 – RP 147+0.000





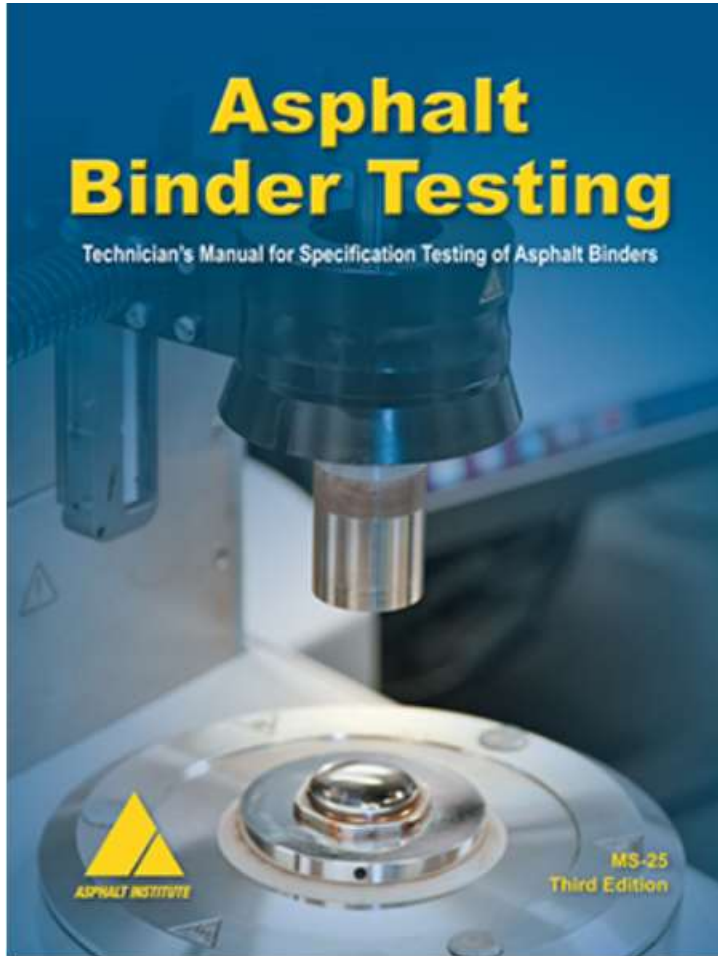
# Performance of US 212 SMA



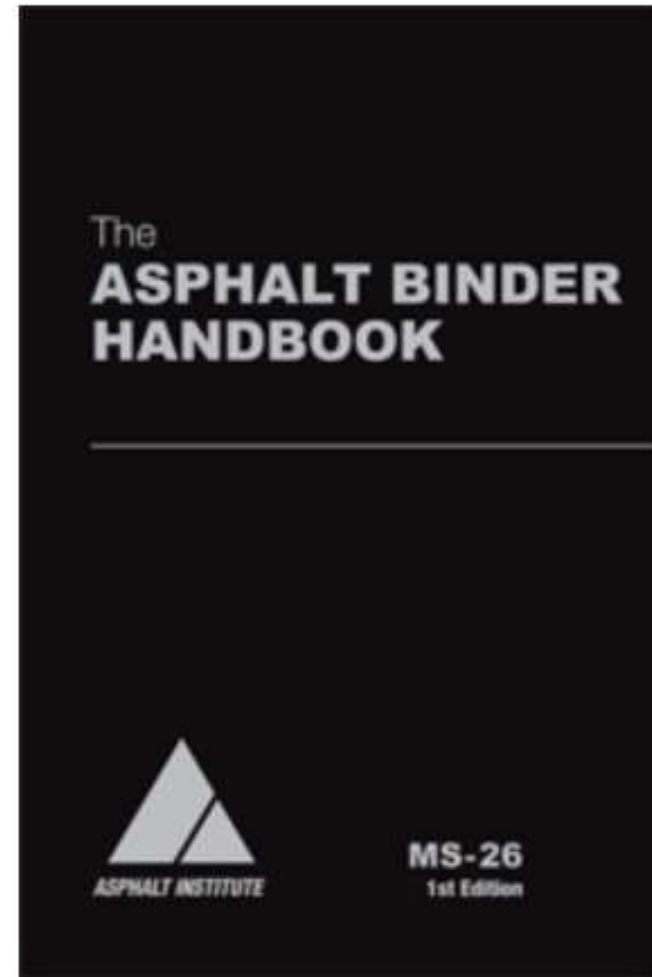
ONE THERMAL CRACK IN 2.7 MILES



# For More Binder Information



MS-25



MS-26

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**Thank You - Questions ?**