Preventive Maintenance, Techniques and Timing North Dakota Asphalt Conference March 31, 2015

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# **The Elected Official**





#### Protecting Our Investment Cost Effectively





#### Highway Capital Improvements

#### Expenditures Needed = \$186 billion annually Current = \$70.3 billion annually

#### Short Fall = \$115.7 billion annually

**Economy** 



# Preservation Expenditures Needed = \$200 billion annually

Highway Pavement & Bridge





#### Lack of Funding

- Last Federal Gas tax 1993
- Of the 18.4 cents about 2.6 goes to Mass Transit
- CPI up 3.36% since 1993
- Meaning \$1 today buys less than \$0.30 worth of 1993 products



#### **Cost of Driving**

- Driving 20,000 miles per year at 20 miles per gallon will equal 1,000 gallons of fuel per year
- 1,000 X \$.184 / gal = \$184.00 per year
  (50 ¢ per day)
- Roads are one of the lowest cost things in our Society!!



Cost of a Gallon...



\* Average Costs November 2014



## Where We Spend Our Money

| Consumer Purchase | Average Monthly Bill |  |
|-------------------|----------------------|--|
| Cable Television  | \$ 123               |  |
| Cell Phone        | \$ 71                |  |
| Internet          | \$ 50                |  |
| Road Taxes        | less than \$ 35      |  |

Road Taxes: (Federal \$15.30 + North Dakota \$ 19.17)







| Preventive Maintenance Applied to HMA Pavements |                      |                      |  |  |  |
|---|----------------------|----------------------|--|--|--|
| Treatment                                       | Treatment Life (yr.) | Life Extension (yr.) |  |  |  |
| Rejuvenator*                                    | NA                   | 3 - 6                |  |  |  |
| Surface Sealer                                  | 0 - 1                | 2 - 4                |  |  |  |
| Crack Sealing                                   | 3 - 8                | 2 - 4                |  |  |  |
| Crack Filling                                   | 2 - 4                | 1 - 3                |  |  |  |
| Slurry Seal                                     | 4 - 5                | 3 - 5                |  |  |  |
| Micro Surfacing - Single                        | 3 – 6                | 3 - 5                |  |  |  |
| Micro Surfacing - Double                        | 4 - 7                | 4 - 6                |  |  |  |
| Chip Seal - Single                              | 3 – 7                | 5 - 6                |  |  |  |
| Chip Seal - Double                              | 5 - 10               | 8 - 10               |  |  |  |
| Ultra-thin Bonded Wearing                       | 7 – 12               | NA                   |  |  |  |
| Dense Graded Thin HMA                           | 5 - 12               | NA                   |  |  |  |
| Open Graded Thin HMA                            | 6 - 12               | NA                   |  |  |  |
| Hot In-place Recycling                          | 6 - 10               | NA                   |  |  |  |
| Cold In-place Recycling                         | 6 - 10               | NA                   |  |  |  |

\* Only certain rejuvenators were considered



#### Typical Life Extensions (Years)

| Treatment       | Good<br>Condition<br>(PCI=80) | Fair<br>Condition<br>(PCI=60) | Poor<br>Condition<br>(PCI=40) |
|-----------------|-------------------------------|-------------------------------|-------------------------------|
| Crack Fill      | 1-3                           | 0 - 2                         | Ο                             |
| Crack Seal      | 2 - 4                         | 1-3                           | Ο                             |
| Fog Seal        | 2 - 4                         | 0 - 1                         | Ο                             |
| Chip Seal       | 5 - 6                         | 3 - 5                         | 0 - 3                         |
| Micro-Surfacing | 4 – 6                         | 3 - 5                         | 1-4                           |
| Thin HMA        | 4 - 10                        | 3 - 7                         | 2 - 4                         |



#### Pavement Condition Index (PCI)



#### Life Extension of Rejuvenators & Asphalt Sealers



lational Center for Pavement

Life Extension



#### **Pavement Selection**





## **Pavement Selection**





#### **Pavement Selection**





#### Framework for Treatment Selection

- Other potential criteria
  - Availability of qualified contractors
  - Availability of materials
  - Time (of year) of construction
  - Pavement noise
  - Facility downtime
  - Surface friction



#### **Asphalt Treatments**



#### **Chemical Properties**

- The causes for aging and deterioration of asphalt binders
- Petroleum Asphalt is comprised of two fractional components Asphaltenes & Maltenes







#### **Maltene Fractions of Asphalt**





 Aging and breakdown of asphalt binders and loss of maltenes begins at the hot-mix plant due to the extreme heating necessary to blend asphalt with aggregate and to get it to the job site in a pliable state.





# Asphalt binder deterioration continues once the mixture is placed on a roadway due to :

- Constant exposure to the Sun's UV rays
- Environmental temperatures
- Oxidation
- Stripping action of storm water and melting snow
- Traffic wear





 Ultraviolet light exposure and the sun's heating effect cause the maltene fractions to be oxidized from the asphalt binder.





#### **Pavement Aged 3-5 Years**





## Pavement Aged 13-17 Years





## **Rejuvenator Selection**





# • Pure maltene based rejuvenators are translucent and leave pavement markings visible with no need for restriping.





#### The long term effectiveness of a maltene based rejuvenator.





#### **Rejuvenator Selection**

#### **Conditions Addressed**

- Oxidation
- Maltine Replenishment
- Moisture Infiltration



Initial Low Skid



### **Asphalt Sealer Selection**





#### Emulsion seals the pavement from moisture, prevent oxidation and provides a temporary blackening of the pavement surface.







• If used on tight, impermeable pavements, the oil may remain on the surface, leaving a surface with poor skid resistance. This is corrected if sand or slag is applied over the treated surface at 1 to 2 lbs/SY.

 The lower skid numbers typically return to normal or acceptable levels within 3-4 days.


## **Asphalt Sealer Selection**

#### **Conditions Addressed**

- Oxidation
- Asphalt Film Thickness
- Initial Raveling
- Moisture Infiltration

#### Limitations

Initial Low Skid



# **Crack Sealing Selection**









Configuration A Standard Reservoir-and-Flush



Configuration B Standard Recessed Band-Aid



Configuration C Shallow Recessed Band-Aid









### Cutting Drums & Cutter Bits





### Carbide Cutter - 4 ¾" Wide Hub





### Random Crack Saw





## **Crack Sealing Selection**

#### **Conditions Addressed**

- Water Infiltration
- Incompressibles

#### **Primary Working Cracks**

- Transverse cracking
- Reflective cracking

#### Limitations

 Must have Clean & Dry Reservoir



# **Crack Filling Selection**





### Melter and Applicator

- Oil-jacketed
- Thermostatic heat controls
- Continuous agitation
- Over-heating safety controls
- Heated hose and wand
- Right size tank capacity for operation



## Melter and Applicator



Tank Agitation





## Swivel Applicator





## **Overband Configuration**





## Treating Edge Joints











## **Crack Filling Selection**

#### **Conditions Addressed**

- Water Infiltration
- Incompressibles
   Non-Working Cracks
   Secondary Cracks
  - Longitudinal cracking
  - Minor block cracking

#### Limitations

 Potential Hot Weather Tracking



## **Slurry Seal Selection**





## Small Cracks & Minor Raveling





### Low Volume Roads & Streets





## **Slurry Seal Selection**

#### **Conditions Addressed**

- Moisture Infiltration
- Longitudinal cracking
- Transverse cracking
- Raveling
- Friction Loss

#### Limitations

Opening to Traffic
 Dependent on Set-Time



## **Micro Surface Selection**









### Micro Surfacing Mix Design

Company Letterhead

Date: April 1, 20XX

RE: Type III CQS-1HP Microsurfacing Mix Design

Dear\_\_\_\_\_

As requested, <u>Testing Company Name</u> prepared a job mix formula according to ISSA accepted testing procedures using Type III aggregate from <u>Company Name</u>, <u>Quarry Name</u>, and the following emulsion CQS-1HP from <u>Company Name</u>, <u>Terminal Name</u>.

The job mix formula based on the data from the laboratory tests is reported as follows. All values are based on dry aggregate weight.

| CQS-1 HP:                     | 12.0 ± 1.0 % |
|-------------------------------|--------------|
| Water:                        | 5.0 - 9.0%   |
| Cement:                       | 0.5 - 1.0%   |
| Residual Content of Emulsion: | 62.4%        |
| Residual AC Content:          | 7.4 ± 0.6 %  |

Test results summarized in this report represent laboratory conditions only. The laboratory tests were performed on materials submitted to this laboratory using accepted procedures. As always, laboratory and field conditions vary significantly due to fluctuations such as temperature and moisture. Care should be taken to adjust material percentages to compensate for any changes.

Sincerely,

John Smith, Chief Chemist



### Micro Surfacing Mix Design

| e Type III   | Vanie, Guan   | ly one  | Emuls, Source:   | Company  | Name, Termir   | nal Name  |
|--|---|---|--|--|--|---|
| 2, 1 <b>3</b> po m   |   |   | Ellius, course,  | Company  | rearies romin  | All reality   |
|  | Pr  | roperties for N   | Aicrosurfacing Mi  | x Design   |  |   |
|  | Fests were r  | un with 12%   | emulsion by dry v  | weight of a  | ggregate   |   |
|  |   |   |  | Lab  |  |   |
| Method   |   |   |  | Results  | Min  | Max   |
| 113 Mixing T   | ime @ 77 %  | -, sec  |  | 180+   | 120  |   |
| ISSA TB 144 Classification Compatibility   |   |   |  |  | 11   |   |
| ISSA TB 139 Wet Cohesion, 30 min, kg-cm  |   |   |  |  | 12   |   |
| ISSA TB 139 Wet Cohesion, 60 min, kg-cm  |   |   | 20   | 20   |  |   |
| 114 Wet Strip  | oping, %  |   |  | >95  | 90   |   |
|  | <i>a</i>  |   |  |  |  |   |
| 10   |   | Asphalt Conte   | ant Optimization I   | Hesults  | • U  |   |
| 1 Uour   | SA IB 100   | Wet Track Ar  | 1alysis, ISSA IB   | 109 Sand   | Adnesion   |   |
| 1-Hour   | 1-Hour  | 6-Day   | 6-Day  | Sand   | Sand   |   |
| Loss, g/ft-  | Spec, g/ft-   | Loss, g/ff  | Spec, g/n-   | Ad., g/ft-   | Spec, g/ft-  |   |
| 41.6   | 50.0  | 251   | 75.0   | 10.0   | 50.0   |   |
| 26.9   | 50.0  | 41.3  | 75.0   | 40.0   | 50.0   |   |
| 14.7   | 50.0  | 29.1  | 75.0   | 46.7   | 50.0   |   |
| 0.8  | 50.0  | 20.2  | 75.0   | 46.7   | 50.0   |   |
| <sup>)</sup>   |   |   |  |  |  | <b>}</b>  |
| ) <del>[</del>   |   |   |  |  |  |   |
| 0  |   | 1   |  |  |  |   |
|  |   |   |  |  |  |   |
| ) <b>†</b>   |   | -1-   |  | -  |  |   |
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| 0<br>0<br>0<br>1   |   |   |  | *  |  |   |
| 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  | 10%   | 11%   | 12%  | 13%  | 14%  | 15%   |
| 0<br>0<br>0<br>  | 10%   | 11% E   | 12%<br>imulsion Content  | 13%  | 14%  | 15%   |
| 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  | 10%   | 11% E   | 12%<br>imulsion Content  | 13%  | 14%  | 15%   |
| 9%   | 10%   | 11% E   | 12%<br>imulsion Content  | 13%  | 14%  | 15%   |
| 0<br>0<br>0<br>9%  | 10%<br>TB 147 Load  | 11% E   | 12%<br>imulsion Content<br>est Lateral Displa  | 13%  | 14%<br>1d Specific Gr  | 15%   |
| ISSA<br>Displace %   | 10%<br>TB 147 Load<br>Spec  | 11% E<br>ded Wheel Te   | 12%<br>Emulsion Content<br>est Lateral Displa<br>Specific<br>Gravity   | 13%  | 14%<br>1d Specific Gr  | 15%   |
| ISSA<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian<br>Jacobian | 10%<br>TB 147 Loa<br>Spec<br>,5.0   | 11% E   | 12%<br>Emulsion Content<br>Post Lateral Displa<br>Specific<br>Gravity<br>1.85  | 13%  | 14%<br>1d Specific Gr  | 15%   |
| ISSA<br>I Lateral<br>Displace. %<br>2.3<br>2.2   | 10%<br>TB 147 Loa<br>Spec<br>5.0<br>5.0   | 11% E   | 12%<br>Emulsion Content<br>est Lateral Displa<br>Specific<br>Gravity<br>1.85<br>1.85   | 13%<br>icement ar<br>Spec<br>2.10<br>2.10  | 14%<br>nd Specific Gr  | 15%   |
|  | April 1, 20X<br>Company I<br>Company I<br>Company I<br>Type III<br>Method<br>113 Mixing Ti<br>144 Classific:<br>139 Wet Coh<br>139 Wet Coh<br>144 Classific:<br>1-Hour<br>Loss, g/ft <sup>2</sup><br>41.6<br>26.9<br>14.7<br>8.0<br>Hour Loss | Company Name, Quar.     E: Company Name, Quar.     E: Type III     Pr     Tests were r      Method     113 Mixing Time @ 77 %     144 Classification Compa 139 Wet Cohesion, 30 m 139 Wet Cohesion, 60 m 139 Wet Cohesion, 60 m 139 Wet Cohesion, 60 m 14 Wet Stripping, %     ISSA TB 100     1-Hour 1-Hour     Loss, g/ft <sup>2</sup> Spec, g/ft <sup>2</sup> 41.6 50.0     14.7 50.0     8.0 50.0     Hour Loss | April 1, 20XA<br>e: Company Name, Quarry Site<br>e: Type III<br>Properties for N<br>Tests were run with 12% of<br>Method<br>113 Mixing Time @ 77 °F, sec<br>144 Classification Compatibility<br>139 Wet Cohesion, 30 min, kg-cm<br>139 Wet Cohesion, 60 min, kg-cm<br>144 Wet Stripping, %<br>Asphalt Conte<br>ISSA TB 100 Wet Track Ar<br>1-Hour 1-Hour 6-Day<br>Loss, g/ft <sup>2</sup> Spec, g/ft <sup>2</sup> Loss, g/ft <sup>2</sup><br>41.6 50.0 251<br>26.9 50.0 41.3<br>14.7 50.0 29.1<br>8.0 50.0 20.2<br>Hour Loss -1-Hour Spec -6-Day Log | Aphil 1, 2000<br>E: Company Name, Quarry Site Emulsion: -<br>E: Type III Emuls. Source:<br>Properties for Microsurfacing Mi<br>Tests were run with 12% emulsion by dry v<br>Method<br>113 Mixing Time @ 77 %, sec<br>144 Classification Compatibility<br>139 Wet Cohesion, 30 min, kg-cm<br>139 Wet Cohesion, 60 min, kg-cm<br>139 Wet Cohesion, 60 min, kg-cm<br>144 Wet Stripping, %<br>Asphalt Content Optimization I<br>ISSA TB 100 Wet Track Analysis, ISSA TB<br>1-Hour 1-Hour 6-Day 6-Day<br>Loss, g/ft <sup>2</sup> Spec, g/ft <sup>2</sup> Loss, g/ft <sup>2</sup> Spec, g/ft <sup>2</sup><br>41.6 50.0 251 75.0<br>26.9 50.0 41.3 75.0<br>14.7 50.0 29.1 75.0<br>8.0 50.0 20.2 75.0<br>Hour Loss -1-Hour Spec 6-Day Loss -6-Day Spec | Applied to the second s | Erulsion: CQS-1HP<br>Emuls. Source: Company Name, Termin<br>Properties for Microsurfacing Mix Design<br>Tests were run with 12% emulsion by dry weight of aggregate<br>Lab<br>Method Results Min<br>113 Mixing Time @ 77 %, sec 180+ 120<br>144 Classification Compatibility 12 11<br>139 Wet Cohesion, 30 min, kg-cm 12 12<br>139 Wet Cohesion, 60 min, kg-cm 20 20<br>114 Wet Stripping, % >95 90<br>Asphalt Content Optimization Results<br>ISSA TB 100 Wet Track Analysis, ISSA TB 109 Sand Adhesion<br>1-Hour 1-Hour 6-Day 6-Day Sand Sand<br>Loss, g/ft <sup>2</sup> Spec, g/ft <sup>2</sup> Loss, g/ft <sup>2</sup> Spec, g/ft <sup>2</sup> Ad., g/ft <sup>2</sup> Spec, g/ft <sup>2</sup><br>41.6 50.0 251 75.0 50.0<br>26.9 50.0 41.3 75.0 40.0 50.0<br>14.7 50.0 29.1 75.0 46.7 50.0<br>8.0 50.0 20.2 75.0 46.7 50.0<br>Hour Loss -1-Hour Spec 6-Day Loss 6-Day Spec Sand Results |



### Micro Surfacing Mix Design

|  |                         |         | Aggregat            | e Analysis Results            |                  |            |
|--|-------------------------|---------|---------------------|-------------------------------|------------------|------------|
| 0:   |                         |         |                     | Dulling Effect                | 1                | 4 11-2 (43 |
| Sleve An<br>Sieve Size                                   | Alysis AAS<br>% Passing | Minimum | and 1 27<br>Maximum | Buiking Effect                | Loose Unit weigr |            |
| 3/8"   | 100                     | 100     | 100                 | 0                             | 103.3            | 103.3      |
| #4   | 85                      | 70      | 90                  | Ĭ                             | 92.4             | 91.5       |
| #8   | 51                      | 45      | 70                  | 2                             | 86.2             | 84.5       |
| #16  | 33                      | 28      | 50                  | 3                             | 83.5             | 81.1       |
| #30  | 25                      | 19      | 34                  | 4                             | 83.1             | 79.9       |
| #50  | 18                      | 12      | 25                  | 5                             | 83.5             | 79.6       |
| #100   | 13                      | 7       | 18                  | 7                             | 86.9             | 81.2       |
| #200   | 8.7                     | 5.0     | 15.0                | 9                             | 93.9             | 86.1       |
| 01   | E an sharal a sa t      | AACUTO  | T 170               |                               |                  |            |
| Sand   | Equivalent              | AASHIO  | 1176                |                               |                  |            |
| Hesuit   |                         | Minimum | Maximum             |                               |                  |            |
|  |                         |         |                     |                               |                  |            |
| 80 -   | . j į.                  | i       | Ì                   |                               |                  |            |
| 80 -<br>60 -<br>40 -<br>20 -                             |                         |         |                     |                               |                  |            |
| 80<br>60<br>40<br>20<br>0<br>50<br>50                    | 0.15                    | 0.6     | Si Si               | eve Size (mm)                 | 4.75             | u<br>o     |
| 80<br>60<br>40<br>20<br>0<br>5000                        | 0.3                     | 0.6     | si<br>Si            | eve Size (mm)                 | 4.75             | ď          |
| 80<br>60<br>40<br>20<br>50<br>80                         | 0.15                    | 0.6     | si<br>Bu            | eve Size (mm)<br>Iking Effect | 4.75             |            |
| 80<br>60<br>40<br>20<br>0<br>20<br>50<br>105.0           | 0.15                    | 0.6     | e<br>Si<br>Bu       | eve Size (mm)                 | 4.75             |            |
| 80<br>60<br>40<br>20<br>520<br>0<br>50<br>105.0<br>100.0 | 0.15                    | 0.6     | Si<br>Bu            | eve Size (mm)<br>Iking Effect | 4.75             | с          |
| 80<br>60<br>40<br>20<br>520<br>0<br>50<br>105.0<br>95.0  | 0.3                     | 0.6     | Si<br>Bu            | eve Size (mm)<br>Iking Effect | 4.76             |            |
| 80<br>60<br>40<br>20<br>520<br>0<br>50<br>95.0<br>90.0   | 0.3                     | 00      | Si<br>Bu            | eve Size (mm)<br>Iking Effect | 4.76             |            |
| 80<br>60<br>40<br>20<br>50<br>105.0<br>90.0<br>85.0      | 0.3                     | 0.6     | si<br>Bu            | eve Size (mm)<br>Iking Effect | 4.75             |            |



### Equipment Calibration to Match Mix Design





## **Micro Surface Selection**

#### **Conditions Addressed**

- Moisture Infiltration
- Longitudinal cracking
- Transverse cracking
- Raveling
- Friction Loss
- Bleeding
- Rutting

#### Limitations

 Mixture subject to reflective cracking



## **Chip Seal Selection**





### Chip Seal 5 Months Old

meteric fire



### Single Chip Seal





### **Double Chip Seal**





### **Pneumatic Rollers**











## **Chip Seal Selection**

#### **Conditions Addressed**

- Moisture Infiltration
- Longitudinal cracking
- Transverse cracking
- Block cracking
- Friction Loss
- Bleeding

#### Limitations

Longer set time



### Framework for Success

### It is the: "right" treatment on the "right" road at the "right" time by the "right" people




## MICHIGAN STATE U N I V E R S I T Y



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